

LT1944

Dual Micropower Step-Up DC/DC Converter

FEATURES

- Low Quiescent Current: 20µA in Active Mode <1µA in Shutdown Mode
- Operates with V_{IN} as Low as 1.2V
- Low V_{CESAT} Switch: 250mV at 300mA
- Uses Small Surface Mount Components
- High Output Voltage: Up to 34V
- Tiny 10-Pin MSOP Package

APPLICATIONS

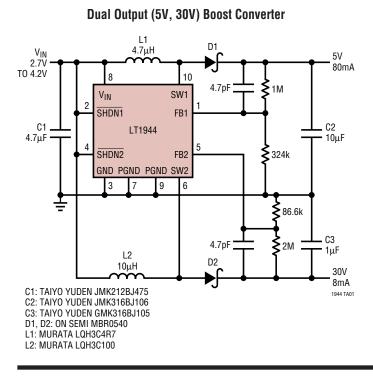
- LCD Bias
- Handheld Computers
- Battery Backup
- Digital Cameras

DESCRIPTION

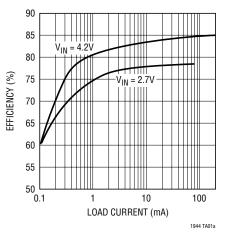
The LT[®]1944 is a dual micropower step-up DC/DC converter in a 10-pin MSOP package. Each converter is designed with a 350mA current limit and an input voltage range of 1.2V to 15V, making the LT1944 ideal for a wide variety of applications. Both converters feature a quiescent current of only 20 μ A at no load, which further reduces to 0.5 μ A in shutdown. A current limited, fixed off-time control scheme conserves operating current, resulting in high efficiency over a broad range of load current. The 36V switch allows high voltage outputs up to 34V to be easily generated in a simple boost topology without the use of costly transformers. The LT1944's low off-time of 400ns permits the use of tiny, low profile inductors and capacitors to minimize footprint and cost in space-conscious portable applications.

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TYPICAL APPLICATION



5V Output Efficiency

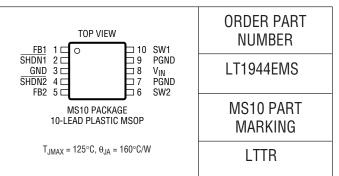


ABSOLUTE MAXIMUM RATINGS

(Note 1)

V _{IN} , SHDN1, SHDN2 Voltage	15V
SW1, SW2 Voltage	36V
FB1, FB2 Voltage	V _{IN}
Current into FB1, FB2 Pins	1mA
Junction Temperature	125°C
Operating Temperature Range (Note 2)4	40°C to 85°C
Storage Temperature Range68	5°C to 150°C
Lead Temperature (Soldering, 10 sec)	300°C

PACKAGE/ORDER INFORMATION



Consult LTC Marketing for parts specified with wider operating temperature ranges.

ELECTRICAL CHARACTERISTICS The \bullet denotes the specifications which apply over the temperature range, otherwise specifications are at T_A = 25°C. V_{IN} = 1.2V, V_{SHDN} = 1.2V unless otherwise noted. The • denotes the specifications which apply over the full operating

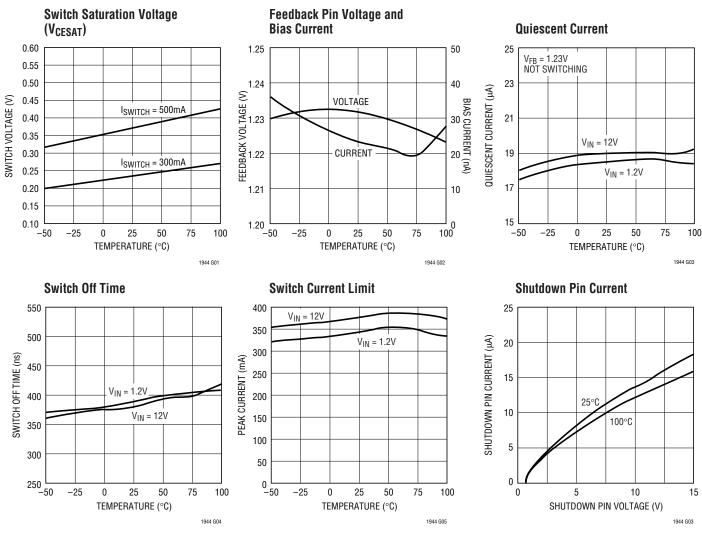
PARAMETER	CONDITIONS		MIN	ТҮР	MAX	UNITS
Minimum Input Voltage					1.2	V
Quiescent Current, Each Switcher	Not Switching V _{SHDN} = 0V			20	30 1	μΑ μΑ
FB Comparator Trip Point		•	1.205	1.23	1.255	V
FB Comparator Hysteresis				8		mV
FB Voltage Line Regulation	1.2V < V _{IN} < 12V			0.05	0.1	%/V
FB Pin Bias Current (Note 3)	V _{FB} = 1.23V	•		30	80	nA
Switch Off Time	V _{FB} > 1V V _{FB} < 0.6V			400 1.5		ns µs
Switch V _{CESAT}	I _{SW} = 300mA			250	350	mV
Switch Current Limit			250	350	400	mA
SHDN Pin Current	V _{SHDN} = 1.2V V _{SHDN} = 5V			2 8	3 12	μΑ μΑ
SHDN Input Voltage High			0.9			V
SHDN Input Voltage Low					0.25	V
Switch Leakage Current	Switch Off, V _{SW} = 5V			0.01	5	μA

Note 1: Absolute Maximum Ratings are those values beyond which the life of a device may be impaired.

Note 2: The LT1944 is guaranteed to meet performance specifications from 0°C to 70°C. Specifications over the -40°C to 85°C operating temperature range are assured by design, characterization and correlation with statistical process controls.

Note 3: Bias current flows into the FB pin.





TYPICAL PERFORMANCE CHARACTERISTICS

PIN FUNCTIONS

FB1 (Pin 1): Feedback Pin for Switcher 1. Set the output voltage by selecting values for R1 and R2.

SHDN1 (Pin 2): Shutdown Pin for Switcher 1. Tie this pin to 0.9V or higher to enable device. Tie below 0.25V to turn it off.

GND (Pin 3): Ground. Tie this pin directly to the local ground plane.

SHDN2 (Pin 4): Shutdown Pin for Switcher 2. Tie this pin to 0.9V or higher to enable device. Tie below 0.25V to turn it off.

FB2 (Pin 5): Feedback Pin for Switcher 2. Set the output voltage by selecting values for R1B and R2B.

SW2 (Pin 6): Switch Pin for Switcher 2. This is the collector of the internal NPN power switch. Minimize the metal trace area connected to the pin to minimize EMI.

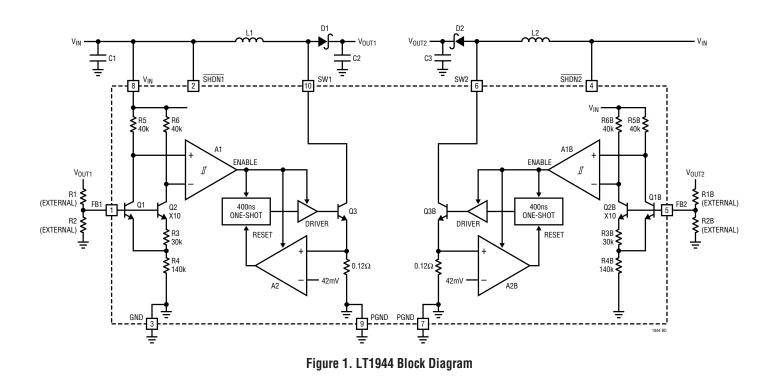
PGND (Pins 7, 9): Power Ground. Tie these pins directly to the local ground plane. Both pins must be tied.

 V_{IN} (Pin 8): Input Supply Pin. Bypass this pin with a capacitor as close to the device as possible.

SW1 (Pin 10): Switch Pin for Switcher 1. This is the collector of the internal NPN power switch. Minimize the metal trace area connected to the pin to minimize EMI.



BLOCK DIAGRAM



OPERATION

The LT1944 uses a constant off-time control scheme to provide high efficiencies over a wide range of output current. Operation can be best understood by referring to the block diagram in Figure 1. Q1 and Q2 along with R3 and R4 form a bandgap reference used to regulate the output voltage. When the voltage at the FB1 pin is slightly above 1.23V, comparator A1 disables most of the internal circuitry. Output current is then provided by capacitor C2. which slowly discharges until the voltage at the FB1 pin drops below the lower hysteresis point of A1 (typical hysteresis at the FB pin is 8mV). A1 then enables the internal circuitry, turns on power switch Q3, and the current in inductor L1 begins ramping up. Once the switch current reaches 350mA, comparator A2 resets the oneshot, which turns off Q3 for 400ns. L1 then delivers current to the output through diode D1 as the inductor

current ramps down. Q3 turns on again and the inductor current ramps back up to 350mA, then A2 resets the oneshot, again allowing L1 to deliver current to the output. This switching action continues until the output voltage is charged up (until the FB1 pin reaches 1.23V), then A1 turns off the internal circuitry and the cycle repeats. The LT1944 contains additional circuitry to provide protection during start-up and under short-circuit conditions. When the FB1 pin voltage is less than approximately 600mV, the switch off-time is increased to 1.5μ s and the current limit is reduced to around 250mA (70% of its normal value). This reduces the average inductor current and helps minimize the power dissipation in the power switch and in the external inductor and diode. The second switching regulator operates in the same manner.



APPLICATIONS INFORMATION

Choosing an Inductor

Several recommended inductors that work well with the LT1944 are listed in Table 1, although there are many other manufacturers and devices that can be used. Consult each manufacturer for more detailed information and for their entire selection of related parts. Many different sizes and shapes are available. Use the equations and recommendations in the next few sections to find the correct inductance value for your design.

PART	VALUE (µH)	MAX DCR (Ω)	VENDOR	
LQH3C4R7 LQH3C100 LQH3C220	4.7 10 22	0.26 0.30 0.92	Murata (714) 852-2001 www.murata.com	
CD43-4R7 CD43-100 CDRH4D18-4R7 CDRH4D18-100	4.7 10 4.7 10	0.11 0.18 0.16 0.20	Sumida (847) 956-0666 www.sumida.com	
D01608-472 D01608-103	4.7 10	0.09 0.16	Coilcraft (847) 639-6400	

0.37

www.coilcraft.com

Table 1. Recommended Inductors

Inductor Selection—Boost Regulator

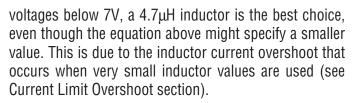
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The formula below calculates the appropriate inductor value to be used for a boost regulator using the LT1944 (or at least provides a good starting point). This value provides a good tradeoff in inductor size and system performance. Pick a standard inductor close to this value. A larger value can be used to slightly increase the available output current, but limit it to around twice the value calculated below, as too large of an inductance will increase the output voltage ripple without providing much additional output current. A smaller value can be used (especially for systems with output voltages greater than 12V) to give a smaller physical size. Inductance can be calculated as:

$$L = \frac{V_{OUT} - V_{IN(MIN)} + V_D}{I_{LIM}} t_{OFF}$$

where $V_D = 0.4V$ (Schottky diode voltage), $I_{LIM} = 350$ mA and $t_{OFF} = 400$ ns; for designs with varying V_{IN} such as battery powered applications, use the minimum V_{IN} value in the above equation. For most systems with output



For higher output voltages, the formula above will give large inductance values. For a 2V to 20V converter (typical LCD Bias application), a 21μ H inductor is called for with the above equation, but a 10μ H inductor could be used without excessive reduction in maximum output current.

Inductor Selection—SEPIC Regulator

The formula below calculates the approximate inductor value to be used for a SEPIC regulator using the LT1944. As for the boost inductor selection, a larger or smaller value can be used.

$$L = 2 \left(\frac{V_{OUT} + V_D}{I_{LIM}} \right) t_{OFF}$$

Current Limit Overshoot

For the constant off-time control scheme of the LT1944, the power switch is turned off only after the 350mA current limit is reached. There is a 100ns delay between the time when the current limit is reached and when the switch actually turns off. During this delay, the inductor current exceeds the current limit by a small amount. The peak inductor current can be calculated by:

$$I_{PEAK} = I_{LIM} + \left(\frac{V_{IN(MAX)} - V_{SAT}}{L}\right) 100 \text{ns}$$

Where $V_{SAT} = 0.25V$ (switch saturation voltage). The current overshoot will be most evident for systems with high input voltages and for systems where smaller inductor values are used. This overshoot can be beneficial as it helps increase the amount of available output current for smaller inductor values. This will be the peak current seen by the inductor (and the diode) during normal operation. For designs using small inductance values (especially at input voltages greater than 5V), the current limit overshoot can be quite high. Although it is internally current



APPLICATIONS INFORMATION

limited to 350mA, the power switch of the LT1944 can handle larger currents without problem, but the overall efficiency will suffer. Best results will be obtained when I_{PEAK} is kept below 700mA for the LT1944.

Capacitor Selection

Low ESR (Equivalent Series Resistance) capacitors should be used at the output to minimize the output ripple voltage. Multilayer ceramic capacitors are the best choice, as they have a very low ESR and are available in very small packages. Their small size makes them a good companion to the LT1944's MS10 package. Solid tantalum capacitors (like the AVX TPS, Sprague 593D families) or OS-CON capacitors can be used, but they will occupy more board area than a ceramic and will have a higher ESR. Always use a capacitor with a sufficient voltage rating.

Ceramic capacitors also make a good choice for the input decoupling capacitor, which should be placed as close as possible to the LT1944. A 4.7μ F input capacitor is sufficient for most applications. Table 2 shows a list of several capacitor manufacturers. Consult the manufacturers for more detailed information and for their entire selection of related parts.

Table 2. Recommended Capacitors

CAPACITOR TYPE	VENDOR	
Ceramic	Taiyo Yuden (408) 573-4150 www.t-yuden.com	
Ceramic	AVX (803) 448-9411 www.avxcorp.com	
Ceramic	Murata (714) 852-2001 www.murata.com	

Setting the Output Voltage

Set the output voltage for each switching regulator by choosing the appropriate values for feedback resistors R1 and R2 (see Figure 1).

$$R1 \!=\! R2 \! \left(\frac{V_{OUT}}{1.23V} \!-\! 1 \right)$$

Diode Selection

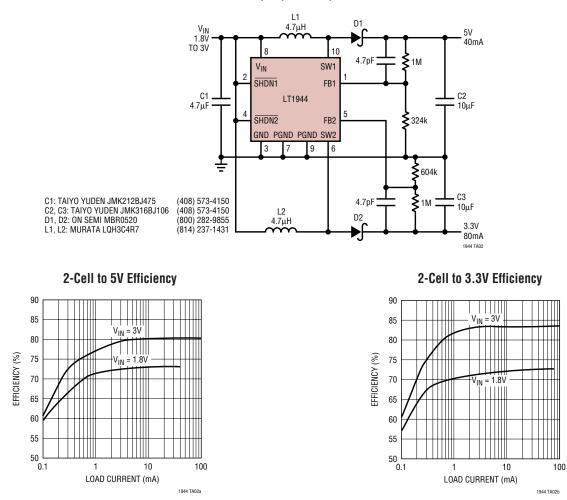
For most LT1944 applications, the Motorola MBR0520 surface mount Schottky diode (0.5A, 20V) is an ideal choice. Schottky diodes, with their low forward voltage drop and fast switching speed, are the best match for the LT1944. For higher output voltage applications the 30V MBR0530 or 40V MBR0540 can be used. Many different manufacturers make equivalent parts, but make sure that the component is rated to handle at least 0.35A.

Lowering Output Voltage Ripple

Using low ESR capacitors will help minimize the output ripple voltage, but proper selection of the inductor and the output capacitor also plays a big role. The LT1944 provides energy to the load in bursts by ramping up the inductor current, then delivering that current to the load. If too large of an inductor value or too small of a capacitor value is used, the output ripple voltage will increase because the capacitor will be slightly overcharged each burst cycle. To reduce the output ripple, increase the output capacitor value or add a 4.7pF feed-forward capacitor in the feedback network of the LT1944 (see the circuits in the Typical Applications section). Adding this small, inexpensive 4.7pF capacitor will greatly reduce the output voltage ripple.

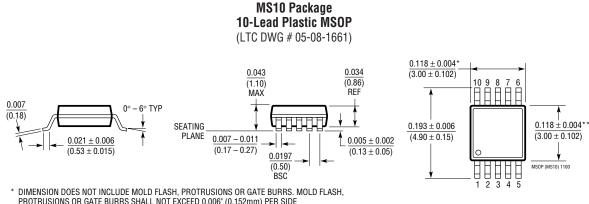


TYPICAL APPLICATIONS



2-Cell Dual Output (3.3V, 5V) Boost Converter

PACKAGE DESCRIPTION



PROTRUSIONS OR GATE BURRS SHALL NOT EXCEED 0.006" (0.152mm) PER SIDE

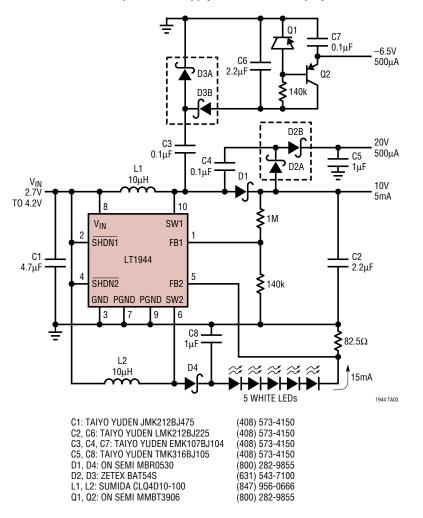
** DIMENSION DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSIONS.

INTERLEAD FLASH OR PROTRUSIONS SHALL NOT EXCEED 0.006" (0.152mm) PER SIDE



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TYPICAL APPLICATION



Four Output Power Supply for Color LCD Displays

RELATED PARTS

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DESCRIPTION	COMMENTS
Single-Cell Micropower 600kHz PWM DC/DC Converter	3.3V at 75mA from One Cell, MSOP Package
Burst Mode [®] Operation DC/DC with Programmable Current Limit	1.5V Minimum, Precise Control of Peak Current Limit
2-Cell Micropower DC/DC with Low-Battery Detector	3.3V at 200mA from Two Cells, 600kHz Fixed Frequency
Single-Cell Micropower DC/DC Converter	3V at 30mA from 1V, 1.7MHz Fixed Frequency
1.4MHz Inverting Switching Regulator in 5-Lead SOT-23	-5V at 150mA from 5V Input, Tiny SOT-23 Package
1.4MHz Switching Regulator in 5-Lead SOT-23	5V at 200mA from 3.3V Input, Tiny SOT-23 Package
Micropower DC/DC Converter in 5-Lead SOT-23	20V at 12mA from 2.5V Input, Tiny SOT-23 Package
Micropower Inverting DC/DC Converter in 5-Lead SOT-23	-15V at 12mA from 2.5V Input, Tiny SOT-23 Package
2.2MHz Boost DC/DC Converter in SOT-23	5V at 450mA from 3.3V, Tiny SOT-23 Package
	Single-Cell Micropower 600kHz PWM DC/DC Converter Burst Mode® Operation DC/DC with Programmable Current Limit 2-Cell Micropower DC/DC with Low-Battery Detector Single-Cell Micropower DC/DC Converter 1.4MHz Inverting Switching Regulator in 5-Lead SOT-23 1.4MHz Switching Regulator in 5-Lead SOT-23 Micropower DC/DC Converter in 5-Lead SOT-23 Micropower DC/DC Converter in 5-Lead SOT-23 Micropower Inverting DC/DC Converter in 5-Lead SOT-23

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